Non-negative Interfacial Tension in Phase-Separated Active Brownian Particles

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We present a microscopic theory for the nonequilibrium interfacial tension γ_{gl} of the free interface between gas and liquid phases of active Brownian particles. The underlying square gradient treatment and the splitting of the force balance in flow and structural contributions is general and applies to inhomogeneous nonequilibrium steady states. We find $\gamma_{gl} \ge 0$, which opposes claims by Bialké *et al.* [Phys. Rev. Lett. **115**, 098301 (2015)] and delivers the theoretical justification for the widely observed interfacial stability in active Brownian dynamics many-body simulations.

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The interfacial tension (or "surface tension") of the free interface between two coexisting bulk phases is one of the most important quantities in the description of a wide range of interfacial phenomena. The tension $\gamma_{\rm gl}$ between coexisting gas and liquid bulk phases plays a particularly central role due to the high symmetry of the coexisting fluid phases. It is a key quantity in the Kelvin equation for capillary condensation, for the strength of the thermal capillary wave spectrum, and for the Laplace pressure in droplets.

The typical values of the interfacial tension vary over many orders of magnitude, when going from molecular to colloidal systems. Using the particle size σ and the thermal energy k_BT as the natural scales, the scaled interfacial tension $\gamma_{\rm gl}\sigma^2/k_BT$ is typically of the order of unity. The dependence on σ is particularly dramatic when going from atoms to colloids. An associated factor of 10^3 of increase in length scale translates into a decrease of $\gamma_{\rm gl}$ by a factor of 10^{-6} , as e.g., theoretically [1–3] and experimentally [4–6] demonstrated in phase separated colloid-polymer mixtures, where confocal microscopy can be used to great effect in studying e.g., droplet coalescence [7] and viscous fingering [8].

Very notably, the existence of the interfacial tension is the mechanism by which macroscopic fluid interfaces, such as in droplets and soap bubbles, attain a minimal geometric shape. The phase separated system minimizes the product of $\gamma_{\rm gl}$ and the interfacial area of the interface. As $\gamma_{\rm gl}$ is independent of curvature in a first approximation, this amounts to minimizing the interfacial area alone. This effect is e.g., commonly exploited in microscopic computer simulation work, where the use of periodic boundary conditions and suitable elongated box geometries offers the system a preferred (short) direction for the choice of interface orientation, and hence a stabilizing mechanism that truncates large scale fluctuations. This also applies to active Brownian particles, i.e., colloids where the diffusive motion is supplemented by directed self-propulsion and

which phase separate at large enough swimming strength [9–12]. Typical experiments rely on catalyzing a chemical reaction to induce such "swimming" [13].

There is much current progress in the description of free equilibrium interfaces, such as e.g., geometry-induced capillary emptying [14], the local structure factor near an interface [15], and Goldstone modes and resonances in the fluid interfacial region [16]. A variety of related deep theoretical topics have been addressed recently, including the curvature dependence of the surface free energy of liquid drops and bubbles [17], the adsorption of nanoparticles at fluid interfaces [18], the free energy of complex-shaped objects [19], the characterization of the "intrinsic" density profile for liquid surfaces [20–22], and the interface tension of curved interfaces [23].

All of the above physical understanding is necessarily based on the fundamental property $\gamma_{\rm gl} \ge 0$. This seemingly indisputable fact was recently challenged based on computer simulation work by Bialké et al. [24] in active Brownian particles. The authors of Ref. [24] used the pressure tensor route and found their results for the interfacial tension to be negative. They argue that this "is a genuine nonequilibrium effect that is rationalized in terms of a positive stiffness." Patch et al. [25] reproduce the negative result using an expression for γ_{gl} similar to that of Ref. [24], but with a different method for calculating the active contribution. From analysis of the interfacial (capillary wave) fluctuations, both groups find a positive value for the interfacial stiffness [24,25]. Lee constructs a coarsegrained model with an effective surface tension that is positive, and he is able to describe his simulation data [26]. Solon et al. [27] in their numerical analysis find a negative value for the tension, but they also state that their framework supports both positive and negative values. Marconi and Maggi [28] state that the tension would turn out to be negative in their theory. Subsequently, Marconi et al. [29] through analytical work have reconsidered the problem of the mechanical derivation of γ_{gl} , but these authors do not report numerical results from their theory and they do not comment on the sign of γ_{gl} in Ref. [29]. Das *et al.* [30] investigated different expressions for the microscopic stress. The authors state that in their treatment the surface tension of active systems can be determined, but they have not done so in Ref. [30]. Considering the influence of activity on the gas-liquid interface of the Lennard-Jones system, Paliwal *et al.* [31] use the pressure tensor route and find a negative contribution from their swim term, but overall positive values for γ_{gl} across a wide parameter range.

Here we demonstrate, based on a nonequilibrium generalization of the microscopic treatment of the interface pioneered by van der Waals [32], that indeed the tension $\gamma_{\rm gl} \geq 0$ for phase-separated active Brownian particles. Its scaled value in natural units is of order unity, and vanishes with a 3/2 (mean-field) exponent near the critical point. This proves, on a sound theoretical footing, the hitherto unexplained stability of the planar active gas-liquid interface and demonstrates the route ahead to the quantitative description of nonequilibrium interfacial properties and phenomena. Our treatment is based on discriminating between structural forces that generate the tension and the flow force balance which does not.

Our mechanism for bulk phase separation is based on the exact translational one-body force balance equation [33,34],

$$\gamma \mathbf{v} = \mathbf{f}_{id} + \mathbf{f}_{int} + \gamma s \boldsymbol{\omega}, \tag{1}$$

where the friction force on the left-hand side is balanced by the ideal diffusive force \mathbf{f}_{id} , the internal force $\mathbf{f}_{\mathrm{int}}$, and the free swim force $\gamma s \boldsymbol{\omega}$ on the right-hand side. The friction constant is indicated by γ and s denotes the constant free swim speed. The velocity \mathbf{v} , the density ρ , \mathbf{f}_{id} , and $\mathbf{f}_{\mathrm{int}}$ all depend on position \mathbf{r} and orientation $\boldsymbol{\omega}$, but not on time as we are considering steady states. Furthermore, we assume (i) the interface between the dense (liquid) and the dilute (gas) phases to be perpendicular to the x axis and (ii) translational invariance with respect to other spatial coordinates. Hence the density varies along the x axis of the system. The ideal diffusive force field is given exactly as $\mathbf{f}_{\mathrm{id}} = -k_B T \nabla \ln \rho$. The internal force field consists of adiabatic and superadiabatic contributions and is defined as

$$\mathbf{f}_{\text{int}} = \mathbf{f}_{\text{ad}} + \mathbf{f}_{\text{sup}} = -\frac{1}{\rho} \left\langle \sum_{i} \delta_{i} \nabla_{i} u(\mathbf{r}_{1}, ..., \mathbf{r}_{N}) \right\rangle, \quad (2)$$

where $\delta_i = \delta(\mathbf{r} - \mathbf{r}_i)\delta(\boldsymbol{\omega} - \boldsymbol{\omega}_i)$ is used as a shorthand notation with δ the Dirac delta function, u indicates the interparticle interaction potential, ∇_i is the derivative with respect to position \mathbf{r}_i of the $i=1,\ldots,N$ particle, and $\langle \cdot \rangle$ is an average in steady state. The adiabatic force field \mathbf{f}_{ad} is defined by the right-hand side of Eq. (2) but taken in an

equilibrium system under the influence of an "adiabatic" external potential that generates the true density profile ρ [35–37]. Here the corresponding equilibrium system has no flow (s=0). Because of the rotational symmetry of the spherical particles considered here \mathbf{f}_{ad} is independent of the particle orientation $\boldsymbol{\omega}$. From classical density functional theory [38], applied to the adiabatic system, it is known that \mathbf{f}_{ad} is a gradient field obtained as $\mathbf{f}_{ad} = -\nabla \mu_{ad}$ [39].

The superadiabatic force field is defined as the difference $\mathbf{f}_{\text{sup}} = \mathbf{f}_{\text{int}} - \mathbf{f}_{\text{ad}}$, cf. Eq. (2). From power functional theory [35] follows that \mathbf{f}_{sup} is a functional of the density profile, but also of the velocity profile.

We split Eq. (1) into a flow equation and a structural equation, given, respectively, by

$$\gamma \mathbf{v} = \mathbf{f}_{\text{flow}} + \gamma s \boldsymbol{\omega},\tag{3}$$

$$0 = \mathbf{f}_{id} + \mathbf{f}_{ad} + \mathbf{f}_{struc}, \tag{4}$$

where the superadiabatic force field is the sum of a flow and a structural contribution, $\mathbf{f}_{sup} = \mathbf{f}_{flow} + \mathbf{f}_{struc}$. The splitting is unique. The superadiabatic flow force field \mathbf{f}_{flow} describes the influence of the internal interactions on the flow. The structural force field \mathbf{f}_{struc} is that part of the total internal force field that influences the spatial structure, together with the adiabatic force field \mathbf{f}_{ad} and the ideal term (which is small in the present situation). Note that it is the functional dependence of \mathbf{f}_{sup} and hence of \mathbf{f}_{struc} on velocity which renders Eq. (4) (highly) nontrivial. Since \mathbf{f}_{id} and \mathbf{f}_{ad} are gradient contributions, \mathbf{f}_{struc} necessarily needs to be a gradient field, $\mathbf{f}_{struc} = -\nabla \mu_{struc}$, which defines μ_{struc} as the negative integral of \mathbf{f}_{struc} . Integrating Eq. (4) in space thus leads to

$$\mu_{\rm id} + \mu_{\rm ad} + \mu_{\rm struc} = \mu_b = \text{const},\tag{5}$$

where μ_b is the constant value in the bulk fluid and the sum determines the total chemical potential. The difference to the equilibrium situation is the dependence of μ_{struc} on the (nonvanishing) flow profile. Conceptually, the three chemical potential contributions play the same role as in equilibrium in that their respective gradient is a force field.

The ideal chemical potential $\mu_{id} = k_B T \ln \rho$ is for simplicity reduced to the orientation-independent expression

$$\mu_{\rm id} = k_B T \ln \rho_0, \tag{6}$$

with the rotational averaged density $\rho_0 = \int d\omega \rho/2\pi$. The approximation is reasonable, since the ideal chemical potential is numerically small in the present situation, as is the corresponding ideal diffusive force (see e.g., Ref. [24]). Furthermore, ρ_0 is a main contribution of the Fourier decomposed density ρ and both densities ρ and ρ_0 coincide in bulk. Since within the used approximations $\mu_{\rm id}$

and μ_{ad} are rotationally invariant, Eq. (5) implies that μ_{struc} and, hence, \mathbf{f}_{struc} are also independent of orientation.

We further discriminate between local and nonlocal contributions in Eq. (5). The ideal chemical potential μ_{id} is a purely local expression and μ_{ad} is also a local term since we base it on a local density approximation. Further nonlocal contributions to μ_{ad} were found to be negligible in the present case. Hence the only considerable nonlocal contribution is contained in μ_{struc} , which we split into a sum of local and nonlocal terms, $\mu_{struc} = \mu_{struc}^{loc} + \mu_{nloc}$. The nonlocal superadiabatic chemical potential is approximated as the lowest order gradient contribution,

$$\mu_{\text{nloc}} = -\nabla \cdot (m\nabla \rho_0) + \frac{1}{2}(\nabla m) \cdot (\nabla \rho_0), \tag{7}$$

where the coefficient m can depend on density ρ_0 and on velocity \mathbf{v} . Note that μ_{nloc} vanishes in both bulk phases due to the constant density $\rho_b = \rho_g, \rho_l$, where ρ_g and ρ_l are the constant densities in the gas and liquid phase. Thus, bulk chemical potential and local chemical potential coincide in bulk, $\mu_b = \mu_{\text{loc}}(\rho_b)$.

For the local chemical potential, $\mu_{\rm loc} = \mu_{\rm id} + \mu_{\rm ad} + \mu_{\rm struc}^{\rm loc}$, the corresponding nonequilibrium local pressure, $P_{\rm loc} = P_{\rm id} + P_{\rm ad} + P_{\rm struc}^{\rm loc}$, can be obtained from the Gibbs-Duhem relation [40]:

$$\frac{\partial P_{\text{loc}}}{\partial \rho_0} = \rho_0 \frac{\partial \mu_{\text{loc}}}{\partial \rho_0}.$$
 (8)

From Eqs. (5) and (7) follows directly that $\mu_{\rm loc}(\rho_l) = \mu_{\rm loc}(\rho_g) = \mu_b$, and using the Gibbs-Duhem relation (8) leads to $P_{\rm loc}(\rho_l) = P_{\rm loc}(\rho_g) = P_b$. The combination of both relations allows us to determine both coexistence densities ρ_g and ρ_l and hence the phase diagram of the system, cf. Ref. [41].

As we have identified the structural gradient force contributions, we can proceed in a purely mechanical way. Hence the gas-liquid interfacial tension is given by [32,38]

$$\gamma_{\rm gl} = \int dx \left(\frac{m}{2} (\nabla \rho_0)^2 - W \right). \tag{9}$$

Equation (9) consists of a nonlocal and a local part. The first, nonlocal contribution results from an (interfacial) square gradient expansion with coefficient m. The second, local term is given as

$$-W = \psi - \psi_b = (\mu_{loc} - \mu_b)\rho_0 - (P_{loc} - P_b), \quad (10)$$

where $\psi = \mu_{\rm loc} \rho_0 - P_{\rm loc}$ and $\psi_b = \mu_b \rho_0 - P_b$ contain the above introduced nonequilibrium (local) chemical potential and pressure. Note that ψ_b is not a constant bulk contribution, since ρ_0 still depends on x. In equilibrium ψ can

be identified as the local Helmholtz free-energy density and ψ_b is the corresponding double tangent line.

The chemical potential balance Eq. (5) can then be rewritten as

$$\frac{\partial W}{\partial \rho_0} + \nabla \cdot (m\nabla \rho_0) - \frac{1}{2}(\nabla m) \cdot (\nabla \rho_0) = 0, \quad (11)$$

where we used Eq. (7) to express the nonequilibrium chemical potential and the derivative of Eq. (10) with respect to density, $-\partial W/\partial \rho_0 = \mu_{\rm loc} - \mu_b$. The first integral with respect to x of Eq. (11) is

$$W + \frac{1}{2}m\left(\frac{\partial\rho_0}{\partial x}\right)^2 = 0,\tag{12}$$

where we used the planar symmetry of the density ρ_0 to simplify the spatial derivative ∇ to $\hat{\mathbf{e}}_x \partial/\partial x$. Rewriting the interfacial tension (9) with relation (12) leads to three alternative forms:

$$\gamma_{\rm gl} = \int_{-\infty}^{\infty} m \left(\frac{\partial \rho_0}{\partial x}\right)^2 dx \tag{13}$$

$$= -2 \int_{-\infty}^{\infty} W dx \tag{14}$$

$$= \int_{\rho_a}^{\rho_l} \sqrt{-2mW} d\rho_0. \tag{15}$$

The numerical values of Eqs. (13)–(15) only coincide if the functions ρ_0 , m, and W are chosen reasonably and satisfy Eq. (12). Thus, whether a choice of these three functions is appropriate can be gauged by the agreement of the value for $\gamma_{\rm gl}$ obtained from either of Eqs. (13)–(15). This provides a check for the approximations for m and W as introduced below.

Equation (13) does not depend on the local contribution W and is thus referred to as the nonlocal route. The relation (14) is independent of the coefficient m of the nonlocal term. It is denoted as the local route, as the integrand is the local quantity W. Expression (15) is called the no-profile route, as it is independent of the density distribution ρ_0 . In practice it can be useful to calculate $\gamma_{\rm gl}$ without knowledge of ρ_0 . In the equilibrium limit of passive particles (s=0) and vanishing particle velocity $\mathbf{v}=0$, our expressions for the interfacial tension coincide with the known equilibrium relations, cf. e.g., Ref. [32].

We apply our general theory for the nonequilibrium interfacial tension to a system of two-dimensional active particles which interact via a Weeks-Chandler-Anderson potential. This is a Lennard-Jones potential cut at its minimum and shifted to be continuous. The corresponding energy scale is ϵ and the characteristic length scale σ is also referred to as the diameter of the spherical particles. The

orientational motion is freely diffusive with rotational diffusion constant k_BT/γ^ω , where γ^ω denotes the rotational friction constant. The rotational averaged density can be approximated with high accuracy as a hyperbolic tangent profile [12],

$$\rho_0(x) = \frac{\rho_g + \rho_l}{2} + \frac{\rho_l - \rho_g}{2} \tanh\left(\frac{x}{\lambda}\right),\tag{16}$$

where λ indicates the interfacial width. The coexistence densities ρ_g and ρ_l were determined from the pressure and chemical potential balance at theoretical coexistence and coincide with results from simulations very well [41,42].

The chemical potential contributions are chosen in accordance with Ref. [41]. The ideal term is given by relation (6). For the adiabatic chemical potential we use the local density approximation on a scaled particle theory for two-dimensional hard disks [43]. This yields

$$\mu_{\rm ad} = k_B T \left[-\ln(1 - \eta') + \eta'(3 - 2\eta')/(1 - \eta')^2 \right], \quad (17)$$

where the rescaled packing fraction $\eta'=0.8\eta$ models the soft Weeks-Chandler-Anderson potential. The packing fraction $\eta=\rho_0/\rho_j$ and $\rho_j=$ const indicates the jamming density, where the motion comes to arrest. The remaining $\mu_{\rm struc}$ corresponds to the quite life chemical potential [41], which in homogeneous bulk is given as

$$\mu_{\text{struc}}^b = \frac{e_1 \gamma \gamma^\omega}{2k_B T} v_b^2 \frac{\rho_b}{\rho_j}, \tag{18}$$

where the strength is determined by the dimensionless constant e_1 . The expression (18) is linear in bulk density ρ_b , quadratic in the bulk speed v_b , and the resulting force acts toward the liquid phase. Note that due to its velocity dependence $\mu_{\rm struc}^b$ is a genuine nonequilibrium expression. To obtain the local structural chemical potential, we expand Eq. (18) across the interface using the orientational averaged density ρ_0 instead of ρ_b and the known linear decrease $v_{\rm loc} = s(1-\rho_0/\rho_j)$ [11] for the speed v_b . This yields

$$\mu_{\text{struc}}^{\text{loc}} = \frac{e_1}{6} \text{Pe}^2 k_B T \left(1 - \frac{\rho_0}{\rho_j} \right)^2 \frac{\rho_0}{\rho_j}, \tag{19}$$

where the introduced Péclet number is $Pe = s\sigma\gamma/k_BT = 3s\gamma^\omega/k_BT\sigma$. This dimensionless constant relates active swimming to rotational diffusion.

The nonlocal chemical potential is approximated in the simplest way, with a constant coefficient $m = e_2 \text{Pe}^2 k_B T / 6 \rho_j^2$, such that Eq. (7) simplifies to $\mu_{\text{nloc}} = -m \nabla^2 \rho_0$ and one obtains

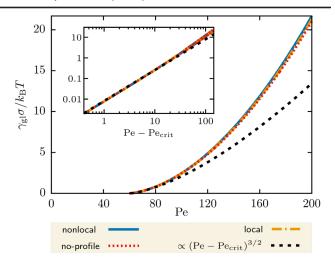


FIG. 1. Interfacial tension $\gamma_{\rm gl}$ determined from the nonlocal route Eq. (13) (full blue line), from the local route Eq. (14) (dash-dotted yellow line), and from no-profile route Eq. (15) (dotted red line) in dependence of the Péclet number Pe. Close to the critical point the tension increases with a critical exponent of 3/2, as indicated by the dashed black line. The inset also shows $\gamma_{\rm gl}$ but in a double-logarithmic plot and the *x* axis is shifted by the critical Péclet number and, hence, is Pe-Pe_{crit}.

$$\mu_{\text{nloc}} = -\frac{e_2 \text{Pe}^2}{6} \frac{k_B T}{\rho_j} \nabla^2 \frac{\rho_0}{\rho_j}, \qquad (20)$$

where the amplitude is determined by the dimensionless constant e_2 . One can show within the power functional framework [33,35] that $\mu_{\rm struc}$ is an intrinsic quantity and can be written as a kinematic functional, hence only dependent on density ρ and velocity ${\bf v}$. Therefore, $\mu_{\rm struc}^{\rm loc}$ and $\mu_{\rm nloc}$ are "naturally"independent of the swim speed and Eq. (19) can be expressed without s as an intrinsic expression [41,44]. The local pressure can be determined straightforwardly from the Gibbs-Duhem relation Eq. (8).

The parameters of the system are chosen as follows. The system is at temperature $k_BT/\epsilon=0.5$, has a rotational friction coefficient $\gamma^\omega/\gamma\sigma^2=1/3$, a jamming density of $\rho_j 2\pi\sigma^2=1.4$, and the dimensionless prefactors $e_1=0.0865$ and $e_2=0.0385$. Requiring e_2 to be constant and the chemical potential balance (5) to be satisfied, the interfacial width λ is determined. The swim speed s changes with Péclet number, $P_0 = s\sigma\gamma/k_BT$, while the other parameters are kept constant. We use the approximations for the orientational averaged density profile ρ_0 , the chemical potential contributions Eqs. (6), (17), (19), and (20), and the corresponding pressures to determine the interfacial tension by evaluating the expressions (13)–(15).

The results from the three methods are displayed in Fig. 1. We find the behavior of the function W and of the interfacial tension to be qualitatively similar to what is found in equilibrium [32]. Figure 1 shows γ_{gl} as a function of Pe. The interfacial tension is only different from zero for

Péclet numbers larger than $Pe_{crit} = 59.3$ [41], when the system phase separates. Here the critical value of the Péclet number [41] is determined by the magnitude of e_1 . The tension increases with rising particle activity and hence with the Péclet number (cf. Fig. 1). Close to the critical point γ_{gl} increases with a critical exponent of 3/2, as indicated by the black dashed line. This corresponds to the theoretical mean-field coefficient of the van der Waals theory, which might be expected since there are many similarities between both descriptions. In order to emphasize the agreement of the interfacial tension with a function proportional to $(Pe - Pe_{crit})^{3/2}$, both quantities are displayed in a double logarithmic plot (cf. the inset of Fig. 1). For Péclet numbers close to the critical point, the functions nearly have the same slope. Far from the critical point the interfacial tension increases faster than with the critical exponent. For a detailed simulation study of the bulk critical behavior of active Brownian particles, see Ref. [45].

The values of the tension are positive, $\gamma_{gl} > 0$, which directly explains the stability of the interface. This is in contrast to Bialké et al. [24], who calculated a negative interfacial tension using the pressure tensor. The results for three different methods, the nonlocal route Eq. (13), the local route Eq. (14), and the no-profile route Eq. (15), agree to a very satisfying degree (cf. Fig. 1). Even far from equilibrium, for example, at Pe = 200, the respective results deviate by only about 3%. This indicates that the chemical potential balance (5) and hence the structural force balance (4) are both satisfied with very good accuracy. Finally, the splitting (3) and (4) [together with (9) within a square gradient approximation] forms a general route toward the interfacial tension of out-of-equilibrium interfaces. We have also ascertained that the "flow" equation of motion (3) creates a vanishing contribution to the interfacial tension in the present system, since after orientational integration the associated pressure tensor contributions either vanish or are isotropic. Hence the splitting (3) and (4) does not imply omission of any relevant terms.

Because of the square gradient character of our treatment, we do not find layering effects at the interface, which would require us to take account of nonlocal interfacial packing effects [20]. Furthermore, our treatment yields the "intrinsic density profile" [21,22], as large scale capillary wave fluctuations are neglected. Thus, interesting future work could be devoted to studying capillary wave fluctuations and the wave vector dependence of the interfacial tension [21,22]. Furthermore, it would be interesting to relate our treatment to that presented in Ref. [27] and to consider fluctuations beyond mean field that could alter the value of the critical scaling exponent.

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- [44] In order to express the swim speed with internal quantities, one can use the forward speed $v_f = \int d\boldsymbol{\omega} \mathbf{J} \cdot \boldsymbol{\omega}/2\pi\rho_0$, the orientational integrated projection of the translational current \mathbf{J} on the particle orientation $\boldsymbol{\omega}$. It is approximately given as $v_f = s(1-\rho_0/\rho_j)/[1+\xi(\nabla\rho_0)^2\rho_0/\rho_j]$ [41], where the constant $\xi>0$ sets the amplitude of a square gradient expansion term. Hence the linear decrease in speed $v_{\text{loc}}=s(1-\rho_0/\rho_j)$ in Eq. (18) can be replaced by the intrinsic expression $v_f[1+\xi(\nabla\rho_0)^2\rho_0/\rho_j]$.
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